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Exterior Cladding Attachment Research

Building America Expert Meeting







Overview

- Cladding Attachment Options
- Cladding Attachment Direct Through Exterior Insulation
- TO2 Building America Research (2011)
- TO3 Building America Research (2012)





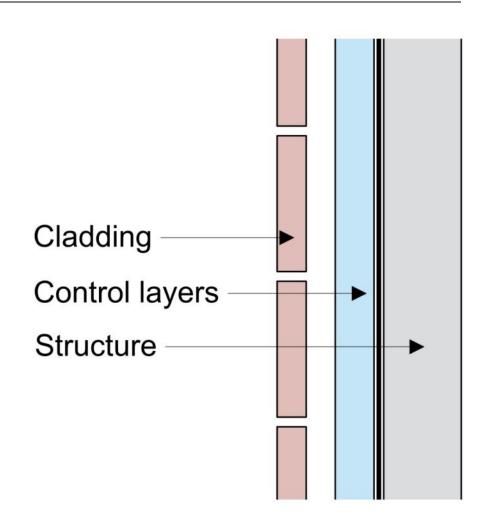
Cladding Attachment Options





Exterior Rigid Insulation

- The "Perfect" Wall
- Increase overall thermal performance
- Minimize thermal bridges
- Minimize potential for air leakage condensation
- Improve air tightness?
- Improve rainwater management?





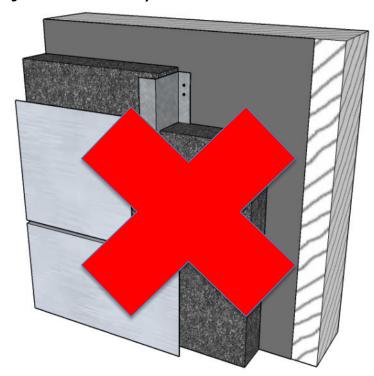


- For insulation 1.5" or less direct attachment of cladding though insulation back to the structure is often practical
- For insulation greater than 1.5" a secondary cladding support system is often needed.
 - Cladding support systems historically done poorly
 - Systems are getting better



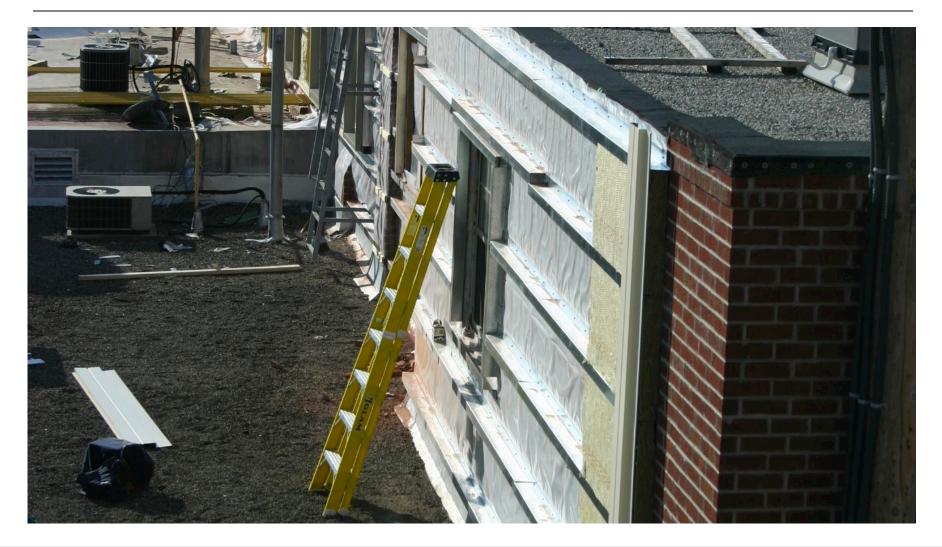


- Single "z-furring"
 - Poor thermal performance (steel stud wall on the exterior – why bother?)





Other Claddings





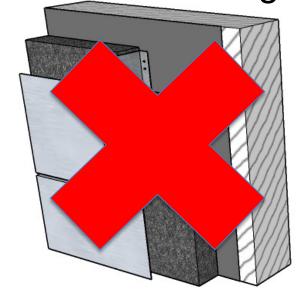


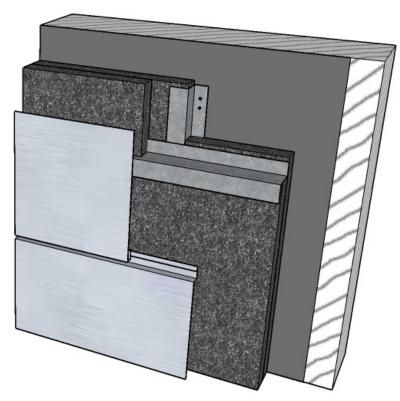
- Single "z-furring"
- Double "z-furring"
 - Can be made to function reasonably well provided that two layers of insulation are used.
 - Often designed with first layer bridging insulation and second layer creating a gap behind the cladding = single "z-furring"





- Single "z-furring"
- Double "z-furring"

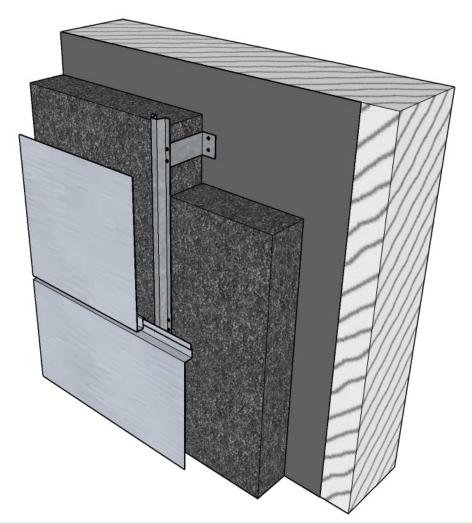






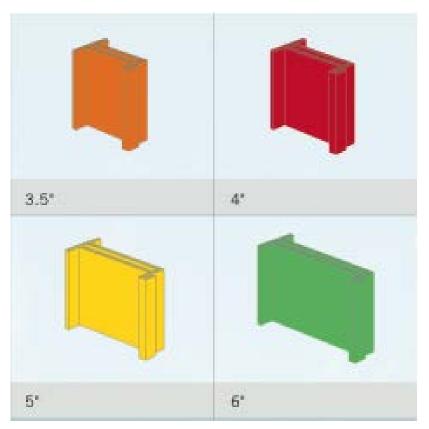


- Single "z-furring"
- Double "z-furring"
- Clip and "z-furring" or hat channel
 - Metal clip
 - Fiberglass clip







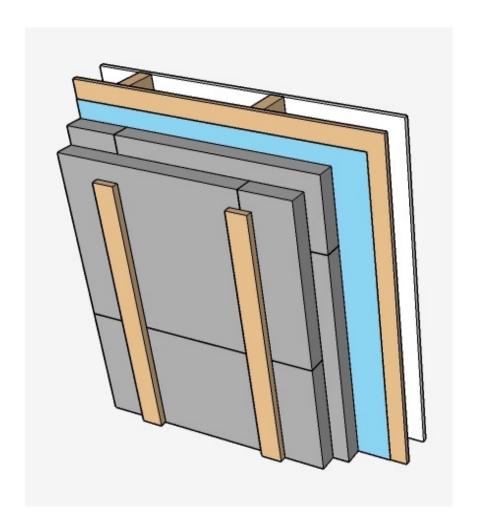






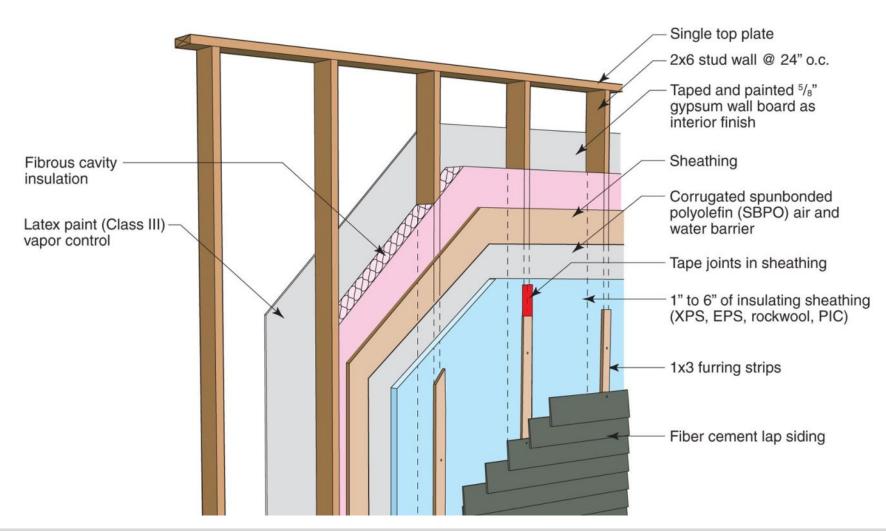


- Single "z-furring"
- Double "z-furring"
- Clip and "z-furring" or hat channel
 - Metal clip
 - Fiberglass clip
- Attach furring directly back to structure through insulation



















Direct Cladding Attachment Through Insulation





- Lots of practical experience with this approach for lightweight cladding systems over thick layers of insulation (several decades).
- Approach has demonstrated very good long term performance
- High resistance from industry





- "Does the insulation provide any additional capacity for the system?"
- BSC staff test







System loaded with air gap between

furring and wall







 System loaded with 4" of rigid mineral fiber insulation between furring and wall

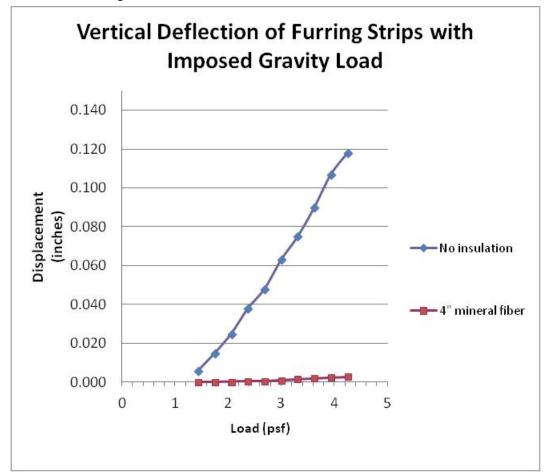








The answer is yes!







- "Does the insulation crush under load?"
- The answer is yes!...
- Loading a system until failure (500lbs to 1000lbs or more per screw fastener) will crush most rigid insulations

.....Unfortunately it is the wrong question



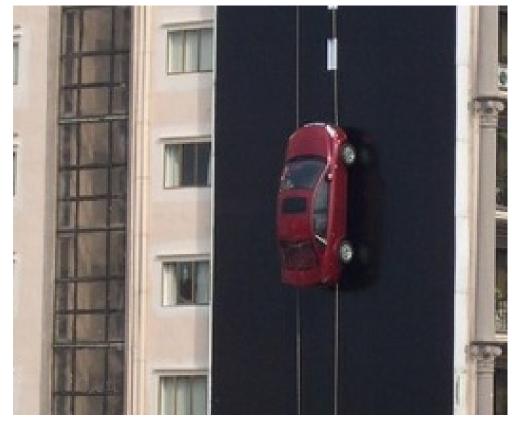


 "Does the insulation crush under a load similar to what will be imposed on it in a cladding support

application?"

■ The answer is no!...

Context is important







Typical cladding weights (psf)

	low	high
Vinyl	0.6	1.0
wood	1.0	1.5
fiber cement	3.0	5.0
stucco	10.0	12.0
adhered stone veneers	17.0	25.0





Typical weights per fastener (lbs)

fastener spacing (in)	16" x 16"	16" x 24"	24" x 24"
area/fastener (ft2)	1.78	2.67	4
vinyl	1.8	2.7	4.0
wood	2.7	4.0	6.0
fibercement	8.9	13.3	20.0
stucco	21.3	32.0	48.0
adhered stone veneers	44.4	66.7	100.0





- Acceptable deflection not ultimate capacity governs
- What is acceptable deflection?
 - Movement a cladding system can accommodate without physical damage or exceeding aesthetic tolerances
- Proposed limits
 - Lap sidings and panel cladding ~ 1/16"
 - Brittle claddings ~1/64" (after initial deflection)





TO2 Building America Research (2011)





Gravity Load Response Testing (2011)

- BSC Research TO2 (DOE Building America Program)
- Short Term and Long Term Deflection Testing
- Multiple insulation types
 - EPS
 - XPS
 - Foil faced polyisocyanurate
 - Rigid mineral fiber





Gravity Load Response Testing (2011)

- Short term testing
- Test panels
 - 4'x8'
 - 1x3 furring spaced 24" oc
 - 16" vertical spacing of fasteners
- Multiple thicknesses
 - 4" and 8" tests







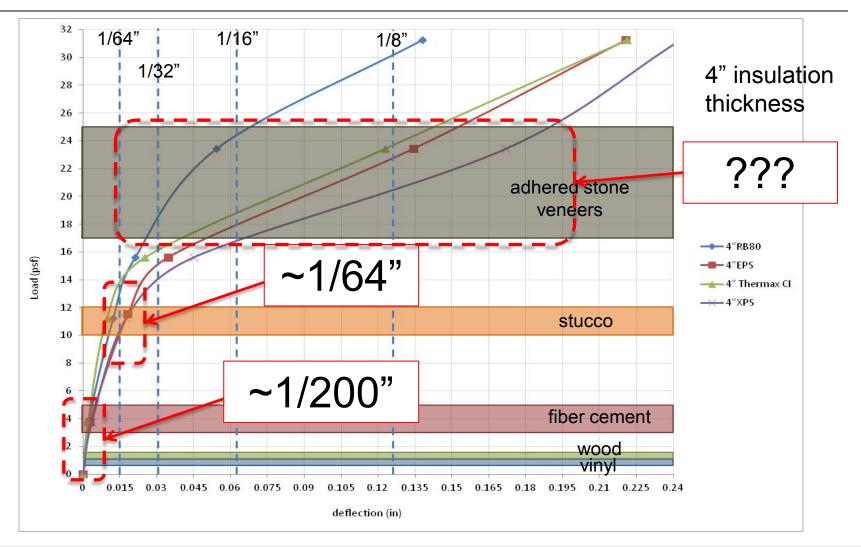
Short-term Gravity Load Response







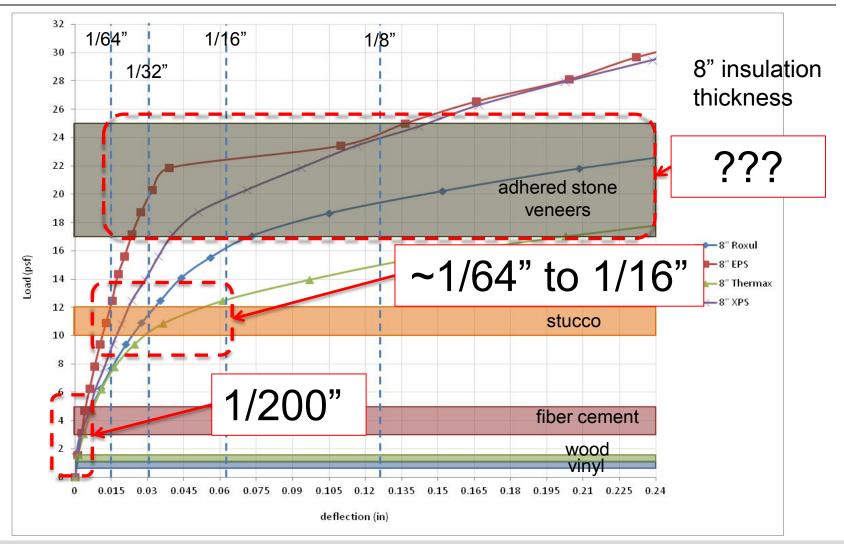
Short-term Gravity Load Response







Short-term Gravity Load Response







Long-term Gravity Load Response

- Long term testing
- Test panels
 - 2'x8'
 - 1x3 furring
 - 16" vertical spacing of fasteners
- Load
 - 13 psf if 24" oc
 - 20 psf if 16" oc
 - 30 lb/fastener







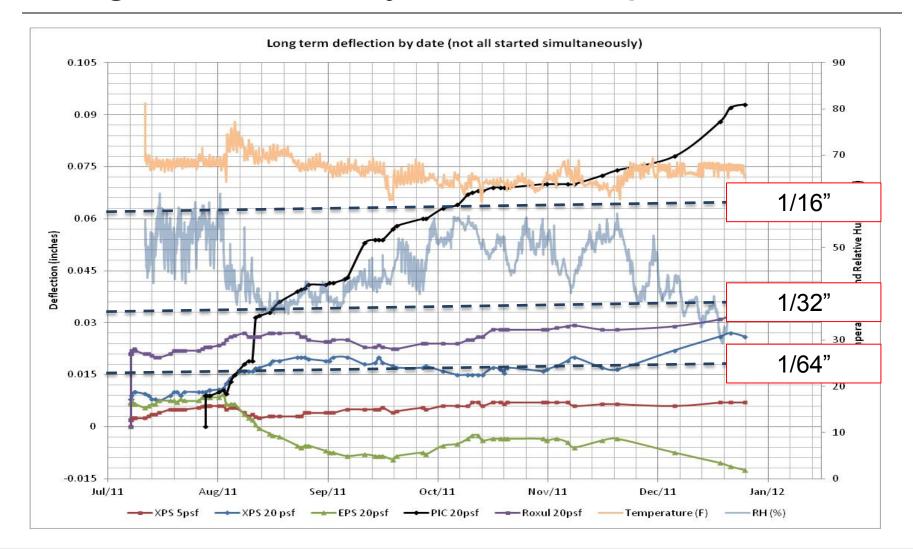
Long-term Gravity Load Response







Long-term Gravity Load Response







Testing Results

- Lightweight claddings (vinyl, wood, fiber cement) have very little movement both under initial loading and long term loading (~1/200")
- For lightweight claddings deflection does not even approach proposed deflection limit (1/16")
- Testing results in line with long history of performance of buildings constructed with this assembly





Testing Results

- Heavier brittle claddings (stucco, adhered stone veneers) initial deflection is not as important as long term deflection
- For stucco claddings (10psf), long term deflection after initial deflection is within proposed deflection limit in stable environmental conditions
- For adhered stone veneer (17psf to 25psf), capacity could be increased with increased fastener spacing.





Additional Questions

- Creep is still not well understood or quantified
- Affected by multiple factors
 - Expansion and contraction of wood
 - Expansion and contraction of insulation
 - Relaxation of wood fibers
 - Plastic deformation of insulation
- Many of these are affected by temperature and relative humidity
- More research is needed to examine the performance of these systems in exposed environments





Additional Questions

- The exact mechanisms of the load deflection resistance are not well quantified
- Discrete load components are theorized but have not been measured
- Important to understand factors that affect the development of system capacity to examine means to design the attachment systems





TO3 Building America Research (2012)





Gravity Load Response Testing (2012)

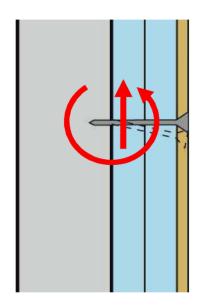
- BSC Research TO3 (DOE Building America Program)
- Discrete Load Component Testing
- Long Term Deflection Testing in Exposed Environment
- Multiple insulation types
 - EPS
 - XPS
 - Foil faced polyisocyanurate
 - Rigid mineral fiber



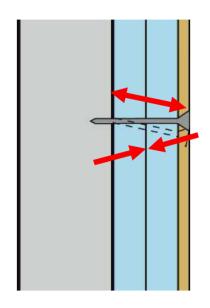


Gravity Load Response Testing (2012)

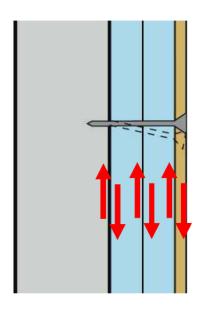
Discrete Load Components



Shear and rotational resistance provided by fastener to wood connections



Rotational resistance provided by tension in fastener and compression of the insulation



Vertical movement resistance provided by friction between layers



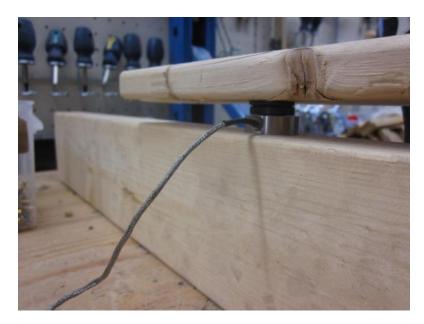


- Series of tests to measure material properties
 - Coefficients of friction
 - Compression modulus of insulation
- Small scale test to try to isolate the discrete functions
 - Screw bending/wood bearing
 - Strut and tie model
 - Friction between layers
 - Due to pre-compression (clamping) forces
 - Due to rotational forces





- Pre-compression (clamping) forces
 - Forces imposed on the system by tightening of the screw fasteners that hold the wood furring in place
 - Tested using common #10 Wood Screws







- Pre-compression (clamping) forces
 - Failure mechanism head pull through of fastener through the furring
 - Preliminary results indicate pretty consistent force magnitudes
 - ~ 150 lbs per fastener with screw head flush with furring surface
 - ~ 180 lbs per fastener with screw over driven
 - Additional testing to be completed to examine relaxation in load over time





- Small Scale Discrete System Tests
 - Custom built test apparatus
 - Intent to evaluate individual force resistance components
 - Screw bending/wood bearing
 - Strut and tie model
 - Friction between layers

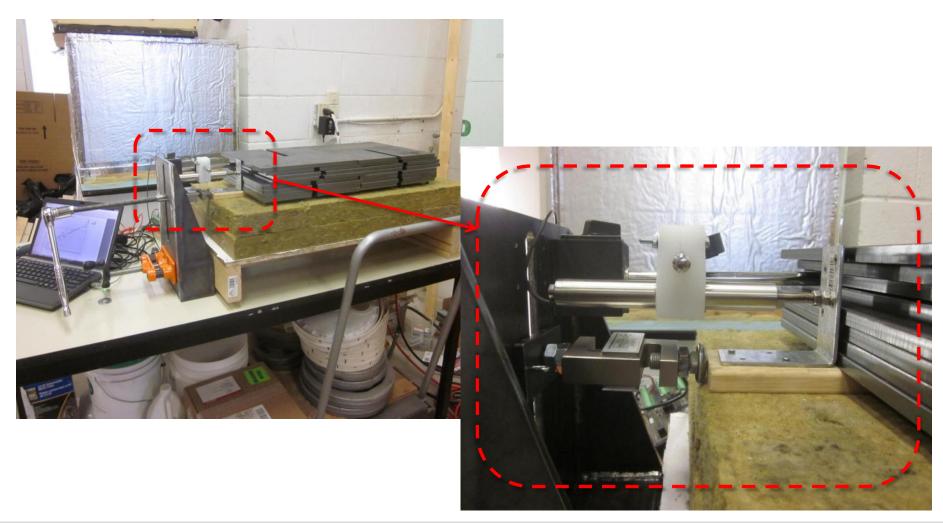
















- Full Scale Wall Assemblies
- Loaded to three representative cladding weights
 - Fiber cement
 - Stucco
 - Cultured stone
- Deflection measured over the course of the year















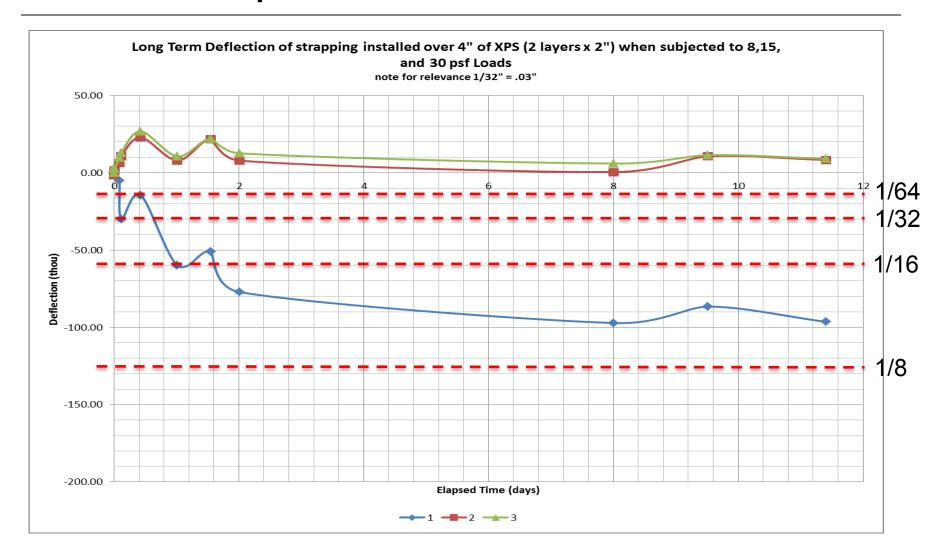






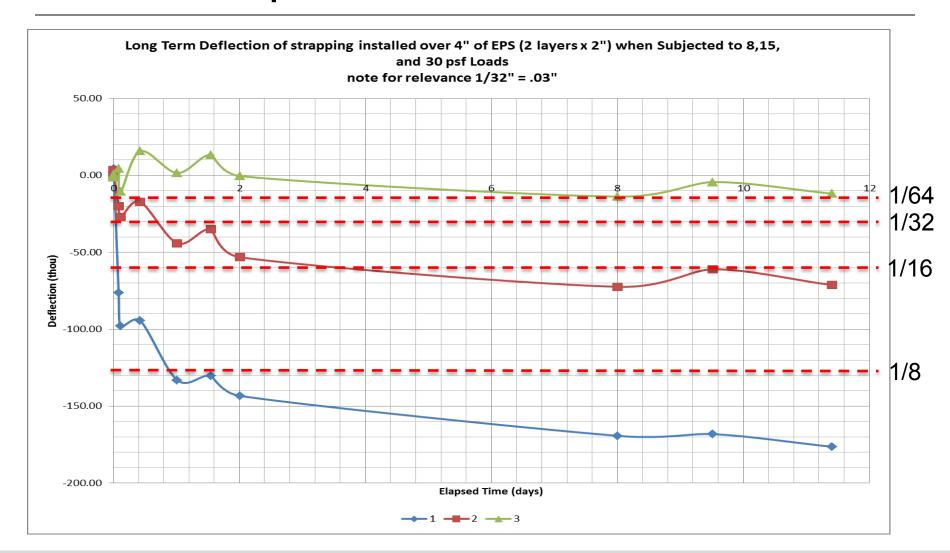
















Testing Results

- Testing is still underway
- Results have not been fully analyzed





Thank you for your time! Any Questions?



